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Errata

Timber Construction Manual, 5th Edition, 1st Printing

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Page	Revision
29	Change word “Transverse” in table heading to “Tangential”
66	Deflection criteria for “Floor beams, ordinary usage” in Table 3.9 should be $l/360$ for applied load only and $l/240$ for applied load plus dead load.
68	Revise Equation 3.8a to: $R = \frac{L^2}{8c} + \frac{c}{2}$
81	Change definition of F_b^* at bottom of page to: “bending design value multiplied by all applicable adjustment factors except C_{fu} , C_L , and C_V , <u>and</u> C_I .”
83	Footnote reference should be changed from “Table 3.3.3” to “Table 4.3”
105	In the last paragraph, change last sentence on page to, “If the end of a beam is beveled (as shown by the dashed line <u>left end of the beam</u> in Figure 4.6), d_e is measured from the inner edge of the support to the bevel.”
108	Change the reference in the first line of text from “Section 4.2.7” to “Section 4.2.8”
111	Revise third paragraph to “1. <i>Check shear.</i> From Section 4.2.7 <u>4.2.8</u> , since the distance...”
111	Revise calculation of shear stress to the following (delete the extra “2” from the denominator): $f_v = \frac{3}{2} \left[\frac{10,800 \text{ lb}}{(5.125 \text{ in.})(17.25 \text{ in.})} \right] = 183 \text{ psi}$
132	Add d_1 to the list of terms in the first line of text following Eq. 4.2.1
133	Change denominator of second term in Eq. 4.24 to the following (close parentheses): “ $F'_{b1} (1 - (f_c / F_{cE1}))$ ”
159	Change the reference in the first line from “Section 4.2.8” to “Section 4.2.9”
159	Change the last term in the denominator to the following (add perpendicular symbol): $(F_b \tan^2 \theta / F_{c\perp})^2$

Page	Revision
166	Change numerator of equation for f_x from “ $2\omega l^2$ ” to “ $3\omega l^2$ ”
183	Equation 4.56 should be: $\Delta_H = \frac{2h\Delta_c}{l}$
186	Change 2 nd equation at top of page to: $\frac{d_c}{R_m} = \frac{69.2 \text{ in.}}{725.6 \text{ in.}} = 0.0954$
252	Change from “ $k_3 = 10.009$ ” to “ $k_3 = 11.36$ ” near center of page
252	Change results of yield mode equations as follows: $Z = \cancel{5322} \underline{4190} \text{ lb}$ mode I _m $= 7529 \text{ lb}$ mode I _s $= \cancel{3216} \underline{2892} \text{ lb}$ mode III_m III _s $= \cancel{4260} \underline{3805} \text{ lb}$ mode IV Mode III _s governs, giving $Z_{30^\circ} = \cancel{3216} \underline{2892} \text{ lb}$.
252	Change equation, bottom of page to: “ $Z' = ZC_D = (\cancel{3216} \underline{2892} \text{ lb})(1.00) = \cancel{3216} \underline{2892} \text{ lb}$ ”
253	Change answer to: “ Answer: The capacity of the given connection for normal load duration is $\cancel{3216} \underline{2892} \text{ lb}$ (mode III _s ; behavior governs).”
255	Font of “p” in Equations 5.14a and 5.14b should be italic, not bold
271	Change 2 nd paragraph, last sentence to “The spacing for the minimum reduced design value, ϵR_{min} , will also be obtained from Table 5.15.”
276	Change equation for row tear-out capacity at bottom of the page to: “ $Z'_{RT} = n \frac{F'_v}{2} A_{\text{crit shear}} = (3)(103.5 \text{ psi})(19.50 \text{ in}^2) = 6055 \text{ lb}$ ”
436	For case 12, 2 nd term in equation for Δ_x should be “ $-3lx^2$ ”
438	For case 17, denominator in equation for Δ_x should be “ $6EI^3$ ”
451	Equation for deflection should be: “ $\Delta = 13.31 \frac{wL^4}{EI} \text{ in.}$ ”
451	First span on drawing should be labeled “L”
453	Equation for M_y should be “ $M_y = \frac{w}{2}(Ly - y^2 - La)$ ” (“y” should not be subscript in first term in parentheses)